

Solar photo-Fenton optimisation in treating carbofuran-contaminated water

Optimización del proceso foto-Fenton solar para el tratamiento de agua contaminada con Carbofurano

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RESUMEN

Se desarrolló una metodología de superficie de respuesta, diseño Box-Benkhen, con el fin de optimizar el proceso foto-Fenton para la degradación de carbofurano ($C_{12}H_{15}NO_3$) usando una planta piloto de colectores solares cilindro-parabólicos. El modelo Box-Benkhen incluyó cuatro variables: porcentaje de degradación de carbofurano, concentración inicial de carbofurano, concentración de peróxido de hidrógeno [H_2O_2] y concentración de hierro [Fe^{2+}]. El proceso de degradación fue monitoreado a través de la concentración de carbono orgánico total y cromatografía líquida de alta resolución. Los resultados mostraron que una concentración de 93,2 mg l⁻¹ de carbofurano se degradó completamente en un tiempo $t_{30W} = 15$ min con 17,1 mg l⁻¹ de Fe^{2+} y 121,6 mg l⁻¹ de H_2O_2 . El proceso foto-Fenton alcanzó 76,7% de mineralización. La biodegradabilidad fue evaluada usando la relación DBO_5/DQO ; este valor incrementó desde 0,04 hasta 0,52 en $t_{30W} = 20$ min, mostrando la posibilidad de usar un tratamiento biológico a partir de ese momento.

Palabras clave: pesticida, carbofurano, foto-Fenton, biodegradabilidad, diseño Box-Benkhen.

ABSTRACT

Box-Benkhen design response-surface methodology was developed to optimise photo-Fenton degradation of carbofuran ($C_{12}H_{15}NO_3$) by using a compound parabolic collector pilot plant. The four variables considered in Box-Benkhen design model included carbofuran degradation percentage, initial carbofuran concentration, hydrogen peroxide [H_2O_2] concentration and iron [Fe^{2+}] concentration. Degradation was monitored by using total organic carbon concentration and high-performance liquid chromatography. A 93.2 mg l⁻¹ carbofuran concentration was completely degraded in $t_{30W} = 15$ min with 17.1 mg l⁻¹ Fe^{2+} and 121.6 mg l⁻¹ H_2O_2 . Photo-Fenton degradation led to 76.7% mineralisation. Biodegradability during optimisation was evaluated by using the BOD_5/COD ratio; this value increased from 0.04 at the beginning of the process to 0.52 in $t_{30W} = 20$ min, thereby showing the effectiveness of using biological treatments.

Keywords: Pesticide, carbofuran, photo-Fenton, biodegradability, Box-Benkhen design.

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Introduction

Wastewater contaminated with pesticides is threatening human health and the environment (Mejía, 2001). Carbofuran (2,3-dihydro-2,2-dimethylbenzofuran-7-yl methyl carbamate $C_{12}H_{15}NO_3$) is an insecticide and nematicide which is included in the general group of carbamate pesticides and is among the great-

est number of pesticide poisonings and deaths around the world (Mahalakshmi, Banumathai *et al.*, 2007; Li-An Lu, Ying-Shin *et al.*, 2010; Katsumata, Matsuba *et al.*, 2005). Carbofuran is the active compound in different commercial pesticides used to control pests and improve productivity of crops like soybeans, rice, sugarcane, tobacco, maize, potatoes and vegetables (Mejía, 2001; RAL-AL, 2008). Cleaning irrigation equipment and empty containers produces large volumes of water contaminated with high concentrations of carbofuran. This wastewater represents serious problems, given the lack of efficient technology treating it and because biological treatments are not able to degrade carbofuran due to its high toxicity and recalcitrance (Li-An, Ying-Shin *et al.*, 2010; RAL-AL, 2008). Technologies must thus be designed to treat this wastewater, destroy recalcitrant substances and cause changes in its chemical structure.

Advanced oxidation processes (AOPs) have been extensively investigated for wastewater treatment. They could be applied as sole treatment or as a pre-treatment to improve pesticide-containing wastewater biodegradability prior to biological treatment. AOPs

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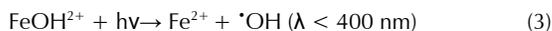
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mainly rely on creating highly oxidative non-selective free radicals, in most cases the hydroxyl radical ($\bullet\text{OH}$) having 2.8V/SHE E° which is effective for persistent pollutant oxidation and mineralisation (Malato, Blanco *et al.*, 2003; Ying-Shih, Chi-Fanga *et al.*, 2010). The Fenton reaction combined with ultraviolet (UV) radiation is one of the most effective methods for degrading organic matter. Fenton reaction with H_2O_2 and Fe^{2+} is shown in equation 1; creating the less powerful hydroperoxyl radical (HO_2^\bullet , E° 1.42 V/SHE) is shown in equation 2 (Li-An Lu, Ying-Shin *et al.*, 2010):



Fenton reaction rate (k_1) is much faster than Fe^{2+} regeneration rate (k_2); therefore, adding Fe^{2+} and H_2O_2 is required to keep the reaction going. The photo-Fenton reaction, a combination of H_2O_2 and UV irradiation below 400 nm with Fe^{3+} or Fe^{2+} , is a promising treatment which can produce relatively more $\bullet\text{OH}$ compared to the Fenton treatment. This is mainly accomplished by photoreduction of $\text{Fe}(\text{OH})^{2+}$ (formed in Fenton reaction pH 2-3) to Fe^{2+} , as shown in equation 3 (Li-An Lu, Ying-Shin *et al.*, 2010). Regenerated Fe^{2+} could undergo further reaction with more H_2O_2 molecules, producing new $\bullet\text{OH}$ and forming a reaction cycle (Chiou, Chen *et al.*, 2006). It has two advantages: facilitating the Fenton treatment without continuous addition of external Fe^{2+} and reducing ferric hydroxide sludge formation (Torrades, Saiz *et al.*, 2008):



Solar photo-Fenton degradation has shown high efficiency in mineralising toxic pesticides and other organic pollutants (Malato, Blanco *et al.*, 2003). The best reaction condition for mineralising target compound must be estimated to avoid wasting chemical reagents and improve process efficiency. Carbofuran degradation using photo-Fenton treatment was optimised in the present study by using a response surface (RS) Box-Benkhen design; the variables to be optimised were initial carbofuran concentration, Fe^{2+} concentration and H_2O_2 concentration. The experiments were performed on CPC pilot scale. Biodegradability parameters were measured during photo-Fenton degradation to identify when photo-treated water would become susceptible to being treated by biological methods.

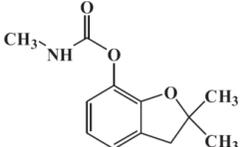
Materials and Methods

Chemicals

Analytical standard carbofuran (Sigma) was used for high-performance liquid chromatography (HPLC) quantification. Table 1 shows the commercial pesticide selected for the degradation experiments. HPLC grade methanol and acetonitrile were supplied by Merck. A Milli-Q ultra-pure water system (Millipore, Milford, MA, USA) was used throughout the study to obtain (HPLC) grade water used in the analysis. Fe^{2+} , as iron sulfate heptahydrate ($\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$) (MOL LABS[®]), was used for the photo-Fenton degradation. Hydrogen peroxide (H_2O_2) reagent grade (30% w/v) from Riedel - De Haën was used. pH was adjusted (between 2.8 - 2.9) with a 2N sulphuric acid solution (H_2SO_4 96% purity from MOL LABS). A 0.1 M sodium bisulphate solution (NaHSO_3) from Riedel-De Haën was used to remove residual hydrogen peroxide to stop the Fenton reaction and preserve the samples. Merckoquant tapes were used for periodic measurement of hydrogen peroxide. pH

was stabilised (between 6 and 8) by drops of a sodium hydroxide solution (2M from MERCK) to precipitate the iron.

Table 1. Model pesticide used for this study.

Active ingredient	Commercial product	Manufacturer	Structure
Carbofuran	Furadan 3SC	Bayer	

Analysis

Carbofuran concentration was measured via liquid chromatography (1 ml/min flow rate) in HPLC-UV (Agilent Technologies series 1100) on a C-18 column (4.6 mm, I.D, 250 mm, from Capital). Water-methanol-acetonitrile (45:35:20) was used as a mobile phase. Mineralisation was followed by measuring dissolved organic carbon (DOC) by direct injection of filtered samples in a Shimadzu-5050A total organic carbon (TOC) analyser and calibrated with standard potassium phthalate solutions.

Biodegradability assays

The BOD5/COD ratio was measured after each photo degradation treatment. Biodegradability was reached when the BOD5/COD ratio was higher than the typical value for domestic wastewater (> 0.4) (Metcalf & Eddy, 1991).

Experimental setup for solar photochemical treatment

Photochemical experiments were performed in sunlight in a CPC pilot plant designed for solar photocatalytic applications (Fig. 1). This reactor was consisted of two modules involving five Pyrex glass tubes; total illuminated area was 1.2 m² and volume 7.8 l.



Figure 1. Photograph of the CPC pilot plant (1.2 m²) used for the photo-Fenton experiments.

22 l of water were re-circulated in the photo reactor at the beginning of each photo-Fenton experiment and the appropriate amount of Furadan was added to reach the initial concentration of the pesticide to be degraded. The pH was then adjusted between 2.8 and 3.0 with concentrated sulphuric acid. Iron salt ($\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$) was added and it was necessary to wait 10 min for homogenisation. An initial hydrogen peroxide dose was added and samples were taken at different times to evaluate carbofuran degradation. The photo-Fenton reaction was verified through the presence of hydrogen peroxide every 5 min; its concentration could not drop below 5 mg/l. UV irradiation in the solar plant was recorded by a radiometer (Davis, Health EnviroMonitorTM). Inci-

dent irradiation could be evaluated regarding time by taking cloudiness and other environmental variations into account. Experiments could thus be compared by using a corrected t_{30W} illumination time (Ballesteros, Casas *et al.*, 2010; Mendoza-Marin, Osorio *et al.*, 2010) by using equation 4:

$$t_{30W} = t_{30W, n-1} + \Delta t_n (UV/30)(V_i/V_t), \Delta t_n = t_n - t_{n-1} \quad (4)$$

where t_n was the experimental time for each sample, UV was the average solar ultraviolet radiation measured during Δt_n , and t_{30W} was "normalised illumination time". Time refers to a constant 30 Wm^{-2} solar UV power (typical solar UV power on a perfectly sunny day around noon). V_t was the total volume of the water loaded in the pilot plant (22.0 l), V_i was total irradiated volume (7.8 l).

Experimental design

A three-factor, three-level Box-Benken design (BBD) was used to determine optimal chemical carbofuran degradation conditions. The method consisted of defining a minimum or low level (denoted as 1), a central or medium level (denoted as 2) and a high or maximum level (denoted as 3) for each experimental factor (Table 2).

Table 2. Three factors selected and three levels.

Levels	$C_{12}H_{13}NO_3$ (mg l ⁻¹)	Fe^{2+} (mg l ⁻¹)	H_2O_2 (mg l ⁻¹)
1	50	3	30
2	100	16.5	115
3	150	30	200

% degradation after $t_{30W} = 15 \text{ min}$

Table 3 shows the matrix design, the conditions and results obtained for each experiment, and the response factor defined as degradation percentage of carbofuran after $t_{30W} = 15 \text{ min}$ followed by HPLC. The data was statically analysed by using Statgraphics software. The experiments were performed randomly to avoid any systematic bias in the outcome (Ray, Lalman *et al.*, 2009). The factors and the experimental levels for each factor were based on values found in the literature, available resources and preliminary experiments' results.

Results and Discussion

Effect of H_2O_2 , Fe^{2+} concentrations on carbofuran degradation

Amounts of H_2O_2 and Fe^{2+} have proven to be two of the most important variables during photo-Fenton degradation (Malato, Blanco *et al.*, 2002; Pignatello, Oliveros *et al.*, 2006). Figure 2 shows the response surface diagram for identifying the best H_2O_2 concentration required in photo-Fenton reaction to degrade a determined amount of carbofuran with $17.1 \text{ mg l}^{-1} Fe^{2+}$ in $t_{30W} = 15 \text{ min}$. It can be noticed in the experimental outcomes that carbofuran degradation increased at higher H_2O_2 concentrations in the range studied here which was mainly due to greater $\bullet OH$ generation (Li-An Lu, Ying-Shin *et al.*, 2010). However, several researchers have also reported the negative effect of H_2O_2 -overdosed photo-Fenton system for the degrading a target compound (Malato, Blanco *et al.*, 2002). At under-overdosed rate, H_2O_2 could react with $\bullet OH$ resulting in less powerful $HO_2\bullet$ being formed, as shown in equation 5. Moreover, $HO_2\bullet$ could further react with $\bullet OH$ and form water and oxygen, as shown in equation 6:

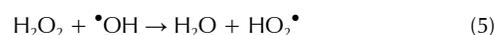


Table 3. Experimental results for Box-Benken design applied to carbofuran oxidation using photo-Fenton degradation.

Run	$C_{12}H_{13}NO_3$ (mg l ⁻¹)	Fe^{2+} (mg l ⁻¹)	H_2O_2 (mg l ⁻¹)	Y experimental (%)	Y calculated (%)
1	100	16.5	115	98.2	97.66
2	150	30	115	89.3	88.15
3	100	30	30	87.38	85.38
4	100	3	30	71.18	69.69
5	100	16.5	115	97.44	97.66
6	100	3	200	92.18	94.17
7	150	3	115	68.5	66.84
8	150	16.5	30	50.1	53.25
9	50	30	115	100	101.66
10	100	30	200	99.88	101.36
11	100	16.5	115	97.34	97.66
12	50	16.5	200	100	96.86
13	150	16.5	200	96.86	96.52
14	50	16.5	30	99.33	99.67
15	50	3	115	98.95	100.09

% degradation after $t_{30W} = 15 \text{ min}$

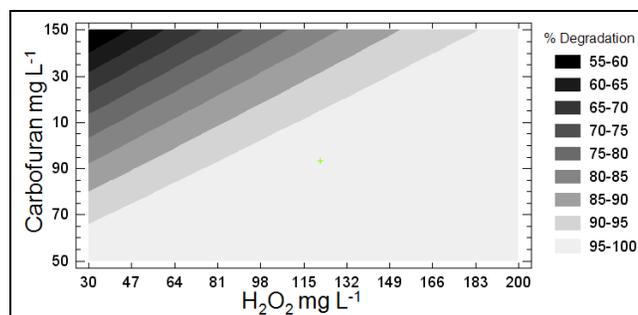


Figure 2. Optimising H_2O_2 concentration for the photocatalytic degradation of carbofuran ($17.1 \text{ mg Fe}^{2+} \text{ l}^{-1}$) using a response-surface diagram. Contours of the response surfaces for carbofuran degradation percentage after $t_{30W} = 15 \text{ min}$.

Figure 3 shows that carbofuran and DOC removal efficiency could be improved by increasing Fe^{2+} concentration. However, using high iron concentrations can be toxic to microorganisms in a biological reactor in coupled systems (Malato, Blanco *et al.*, 2002); it produces ferric hydroxide sludge which can produce areas in the photo-reactor reducing solar light incidence and making it necessary to design another treatment for iron removal, thereby making the system more complex and expensive (Ballesteros, Casas *et al.*, 2010; Mendoza-Marin, Osorio *et al.*, 2010; García-Montaño, Torrades *et al.*, Oliveros *et al.*, 2006; Malato, Fernández *et al.*, 2009).

Optimising photo-Fenton degradation applied to carbofuran degradation

Figure 4 shows analysis of experimental results using a Pareto graph. The Pareto diagram was used to draw more significant conclusions regarding these variables and interactions. This graph shows the magnitude and importance of the effects (variables and

interactions). It displays the absolute value of the effects on the ordinate and standard pseudo-error of the effects on the abscissa (95% confidence interval). The Pareto chart has a reference line (solid vertical line) and any effect surpassing this line was potentially important. The reference line was simultaneous margin of error. The signs + and - represented positive and negative effects. A positive effect indicated that carbofuran degradation increased in the presence of high levels of the respective variables within the range studied while a negative effect indicated that carbofuran degradation increased in the presence of low levels of these variables. Positive quadratic order polynomial coefficients indicated a synergistic effect, while negative coefficients indicated an antagonistic effect between or among the variables (Giraldo, Peñuela et al., 2010).

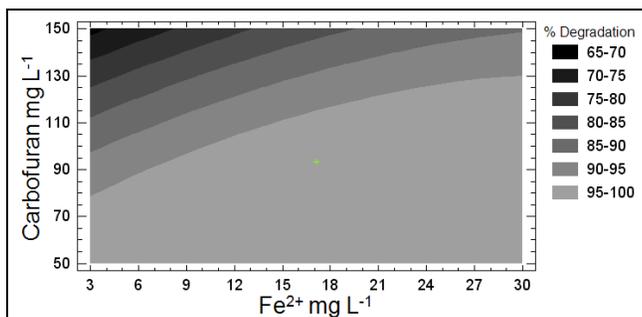


Figure 3. Optimising the Fe²⁺ load for the photocatalytic degradation of carbofuran (121.6 mg H₂O₂) using a response-surface diagram. Contours of the response surfaces for carbofuran degradation percentage after t_{30w} = 15 min.

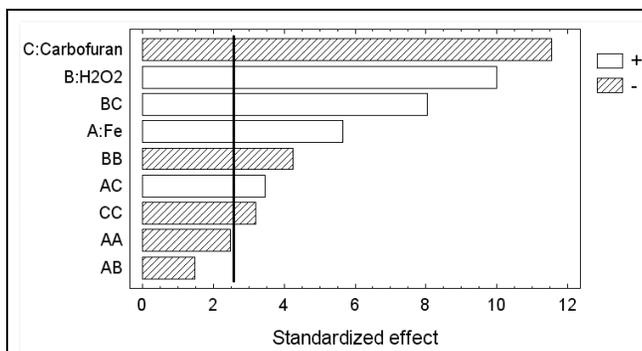


Figure 4. Pareto chart for carbofuran degradation by photo-Fenton t_{30w} = 15 min. Figure obtained according to the experimental data presented in Table 3.

Experimental design methodology led to producing a reduced model directly relating response factors to influential variables. The reduced model's coefficients in polynomial expression were calculated by multiple regression analysis using Statgraphics Plus 5.1 software and representing the weighting for each variable. Optimal conditions could also be represented in polynomial expression (7), where Y (%) represented carbofuran degradation percentage after t_{30w} = 15 min:

$$\begin{aligned}
 Y(\%) = & 103,915 + (0,575 * Fe) + (0,0793 * H_2O_2) - (0,284 * C_{12}H_{15}NO_3) \\
 & - (0,020 * Fe^2) - (0,002 * Fe * H_2O_2) \\
 & + (0,007 * Fe * C_{12}H_{15}NO_3) - (0,001 * H_2O_2^2) \\
 & + (0,003 * H_2O_2 * C_{12}H_{15}NO_3) - (0,002 * C_{12}H_{15}NO_3^2)
 \end{aligned}
 \tag{7}$$

The negative quadratic factors for carbofuran, hydrogen peroxide and iron concentration in the polynomial expression corroborated the fact that these concentrations' load was an intermediate value

in the range being tested. Higher carbofuran concentration values reduced its degradation as time elapsed whereas greater amounts of hydrogen peroxide and iron led to more successful carbofuran degradation.

According to the response-surface diagrams (Fig. 2 – Fig. 3) and equation 7, the optimal combination of factors at t_{30w} (15 min) for obtaining 100% carbofuran degradation is shown in Table 4.

Table 4. Optimising carbofuran oxidation via photo-Fenton degradation.

Factor	Lower (mg l ⁻¹)	Higher (mg l ⁻¹)	Optimum (mg l ⁻¹)
A (Fe ²⁺)	3	30	17.1
B (H ₂ O ₂)	30	200	121.6
C (C ₁₂ H ₁₅ NO ₃)	50	150	93.2

% degradation after t_{30w} = 15 min.

To verify the validity of the equation model, Table 3 also indicates the estimated values for carbofuran degradation percentages calculated by equation 7. It should be noted that estimated values were close to those of the experimental data. Indeed, R² and the reproducibility obtained by Statgraphics Plus 5.1 software were 98.7% and 96.3%, respectively. These results verified the model's validity.

Carbofuran degradation in optimised conditions

Figure 5 shows a new set of experiments carried out in optimised conditions: 93.2 mg l⁻¹ C₁₂H₁₅NO₃, 17.1 mg l⁻¹ Fe²⁺, and 121.6 mg l⁻¹ H₂O₂. The totality of carbofuran was eliminated after t_{30w} = 15 min. Optimal carbofuran concentration was given different treatments (photolysis, optimal Fe²⁺ concentration + UV and optimal H₂O₂ concentration + UV) to analyse each factor's inference on carbofuran photo-treatment. The results indicated that initial carbofuran concentration was removed after t_{30w} = 15 min; 65% mineralisation occurred after this time. Carbofuran degradation was higher in the experimental H₂O₂ concentration + UV than in the experimental Fe²⁺ concentration + UV. This could be explained by using equation 3 in which one H₂O₂ molecule reacted with solar radiation below 310 nm to produce two •OH molecules (Malato, Blanco et al., 2003). Water has small amounts of iron which, together with hydrogen peroxide, promoted •OH formation (Malato, Fernández et al., 2009).

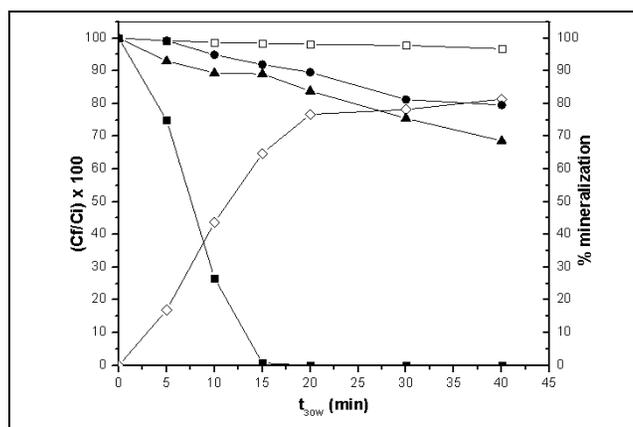


Figure 5. Carbofuran evolution (93.2 mg l⁻¹), by photolysis (□), UV+Fe²⁺ (●), H₂O₂+UV (▲) and photocatalysis (■), mineralisation of dissolved organic carbon (DOC) (◇) during photo Fenton degradation in optimised conditions. Initial COD 320 mg l⁻¹; initial DOC 120 mg l⁻¹.

Photo-treated water's average oxidation state (AOS) (Eq. (8)) and COD/DOC ratio were determinant in photo-treated wastewater to evaluate photocatalytic effect on biodegradability and determine the minimum time necessary to increase wastewater biodegradability; both parameters were considered indirect measurements of probable biodegradability (Sitori, Zapata *et al.*, 2009; Katitvichyanukul and Suntronvipart, 2006):

$$\text{AOS} = \frac{4(\text{DOC} - \text{COD})}{\text{DOC}} \quad (8)$$

The AOS ranged from +4 for CO_2 , representing the most oxidised state of carbon, to -4 for CH_4 . Figure 6 shows that AOS increased during the first 20 normalised minutes (t_{30W}) until it reached a stable 1.3 value. This increase suggested oxidation reactions present during photo-Fenton degradation and intermediate products' chemical nature did not change significantly after 20 minutes. It was also observed that the COD/DOC ratio value decreased, confirming that the species were oxidised. The COD/DOC ratio was normalised at $t_{30W}=20$ min, indicating that the species reached a point where oxidation and mineralisation became stabilised. According to carbofuran degradation pathways by photo-Fenton (Li-An Lu, Ying-Shin *et al.*, 2010), mineralisation increased by up to 76.7% $t_{30W}=20$ indicating that the furan ring or benzene ring was opened and, subsequently, mineralised to inorganic carbon dioxide and water via carbamic acid and methyl amine. The sub-products formed during this stage were highly oxidised short-chain organic compounds; such compounds are difficult to oxidise but are usually biodegradable (Laperlot, Pulgarin *et al.*, 2006).

It has been shown that some more toxic and recalcitrant species than the initial compound can appear after treatment; these species are thus impossible to remove through common biological treatment (Mendoza-Marin, Osorio *et al.*, 2010). Figure 7 shows the change in BOD5/COD ratio with exposure to sunlight. The initial BOD5/COD ratio was 0.04, indicating that the organic matter in the water was not biodegradable, and after $t_{30W} = 20$ min its value reached 0.52, meaning that all carbofuran content had to be removed because even a low carbofuran concentration is very toxic for microorganisms.

Conclusions

It was found that the effluent obtained after photo-Fenton degradation was able to continue to complete decontamination via biological treatment.

Photocatalysis ($t_{30W} = 20$ min) led to efficient mineralisation (76.7%) of organic-load in these types of discharge with low reagent consumption facilitating its industrial application.

It has been demonstrated that biological treatments cannot be applied while amounts of carbofuran remain due its high toxicity, even at low concentration. Photo-treatment must totally degrade carbofuran concentration. Biological systems should only be used to treat photo degradation products of carbofuran.

The Box-Benken experimental design allowed a constant carbofuran value to be eliminated to obtain optimal iron and hydrogen peroxide values to avoid unnecessary reagent use and avoid additional processes for removing residual reagents.

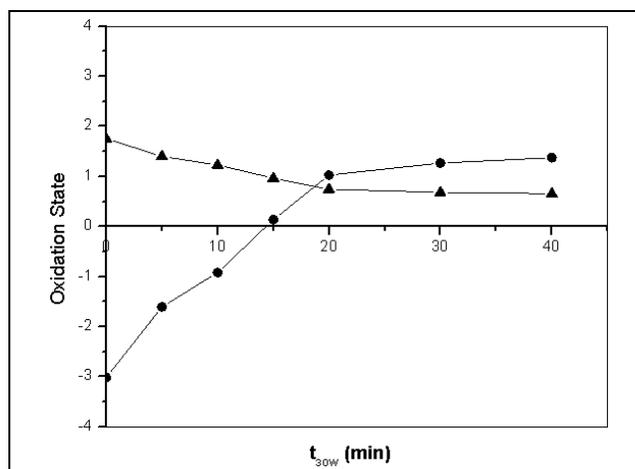


Figure 6. The COD/DOC ratio (▲) and the AOS (●) during photo-Fenton degradation in optimised conditions.

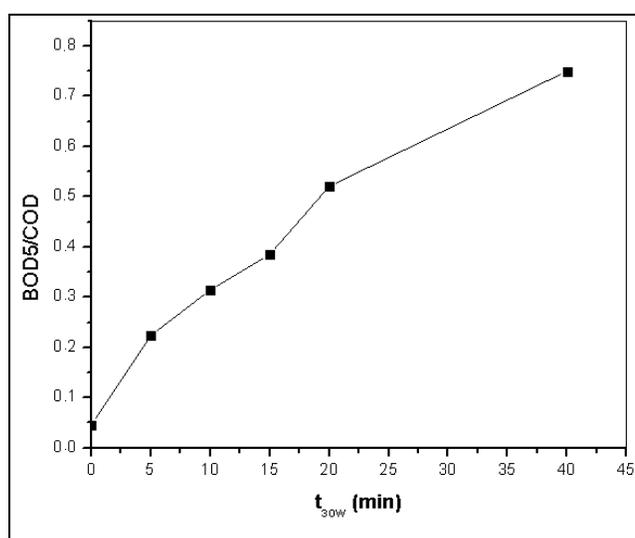


Figure 7. The BOD5/COD ratio during photo-Fenton degradation in optimised conditions.

Acknowledgments

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